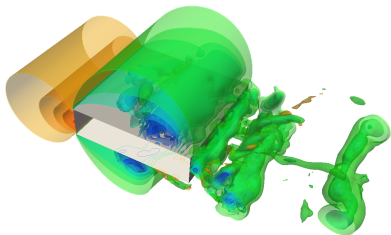


# Comparison of numerical and experimental $C_p$ on a 4:1 rectangular cylinder

A. Guissart, T. Andrianne, G. Dimitriadis and V.E. Terrapon

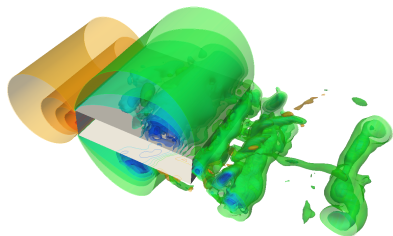
Department of Aerospace and Mechanical Engineering  
University of Liège

EACWE - 4 July 2017



## Context

- flow around a 4:1 rectangular cylinder
- numerical and experimental studies
- moderate  $Re$  and different  $\alpha$



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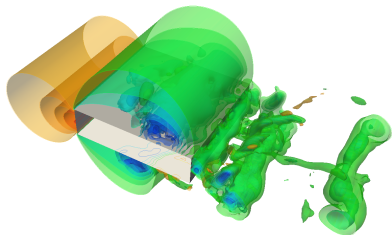
## Objectives

- determine the effects of  $\alpha$  on the flow features and the aerodynamic loads
- assess the capability of URANS and DDES to provide an accurate estimation of the flow and the aerodynamic loads

# Methodology

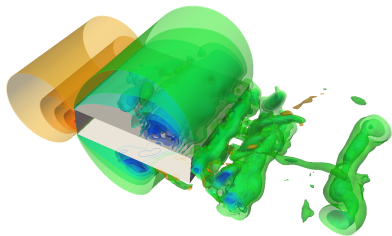


# Methodology



Flow studied through EXP and CFD

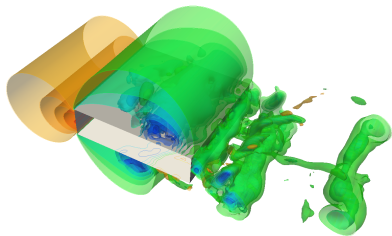
# Methodology



Flow studied through EXP and CFD

dynamic pressure measurements  
for different  $Re$  and  $\alpha$

# Methodology



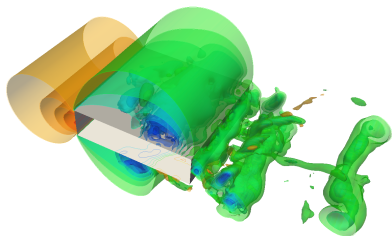
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2D URANS using  $k - \omega$  SST model  
for different  $\alpha$

3D DDES using SA model  
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Comparison of  
EXP and CFD results

- statistics on  $C_p$ ,  $C_l$ ,  $C_d$ ,  $C_m$  and  $St$
- dynamic mode decomposition (DMD) on unsteady  $C_p$

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- DMD<sup>a</sup> = decomposition in single frequency spatial modes

$$\mathbf{v}_1^N(\mathbf{x}, t) = \sum_{k=1}^K \underbrace{q_k^{DMD}}_{\text{amplitude}} \underbrace{\phi_k^{DMD}}_{\text{spatial mode}} \underbrace{\exp(\lambda_k^{DMD} \mathbf{t})}_{\text{time evolution}} \quad \text{with } \mathbf{v}_1^N = [C_p \ C_l \ C_d \ C_m]^T$$

<sup>a</sup>“Dynamic mode decomposition of numerical and experimental data” by Schmid (2010)

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- DMD is used to reconstruct an approximation of the results

$$\hat{\mathbf{V}}_1^N = \sum_{k^{\text{th selected mode}}} q_k^{DMD} \phi_k^{DMD} \exp\left(\Im(\lambda_k^{DMD}) \mathbf{t}\right)$$

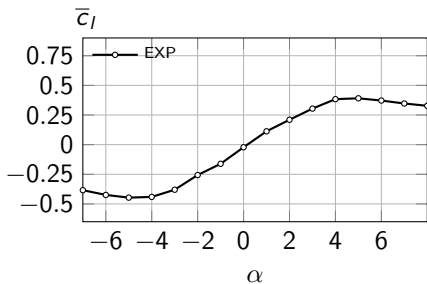
- selected modes correspond to the mean of  $\mathbf{V}_1^N$  and the mode associated to the shedding frequency

<sup>a</sup> "Dynamic mode decomposition of numerical and experimental data" by Schmid (2010)

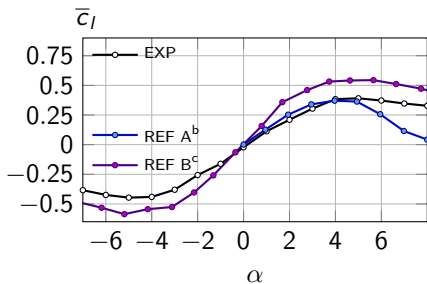
# Results



# Results: mean load coefficients and $St$



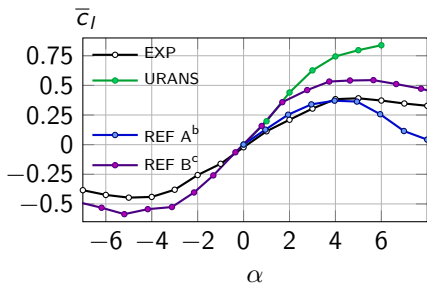
# Results: mean load coefficients and $St$



<sup>b</sup> "Aeroelastic instability of rectangular cylinders in a heaving mode" by Washizu et al. (1978)

<sup>c</sup> "Torsional flutter of rectangular prisms" by Nakamura and Mizota (1975)

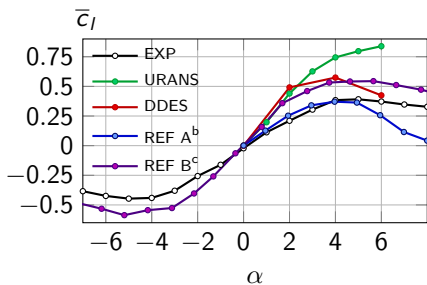
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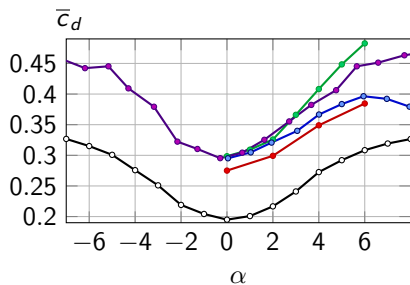
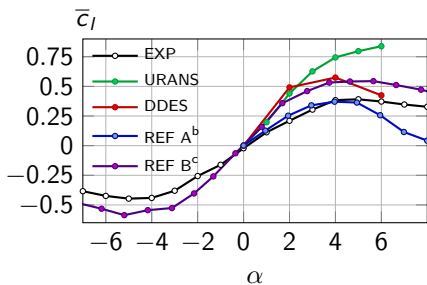
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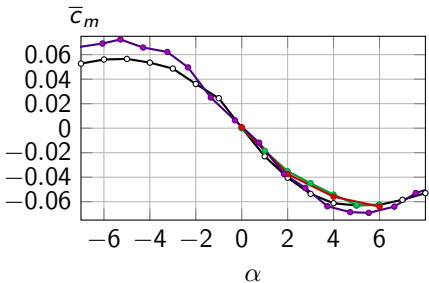
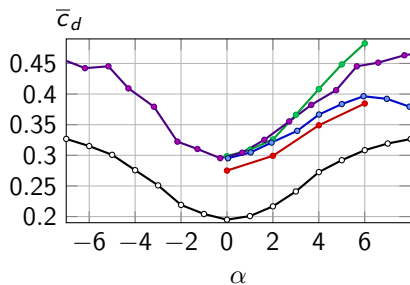
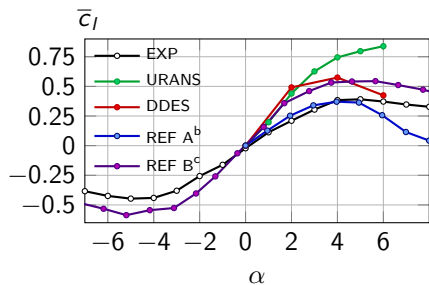
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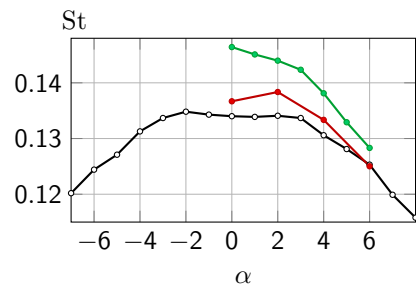
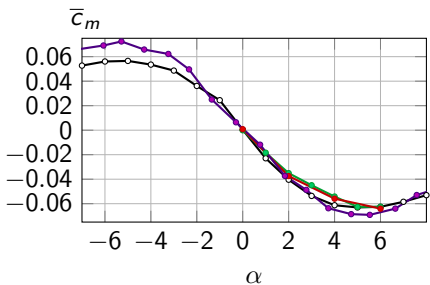
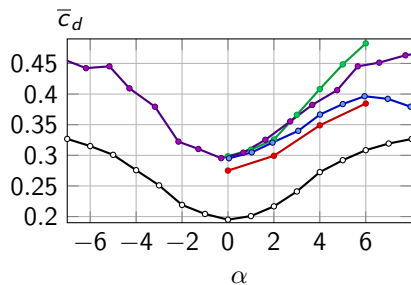
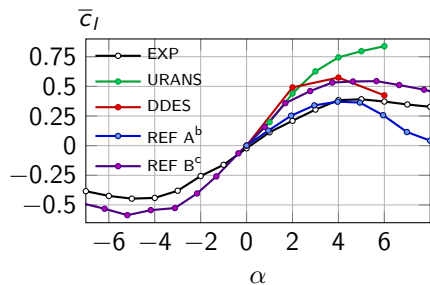
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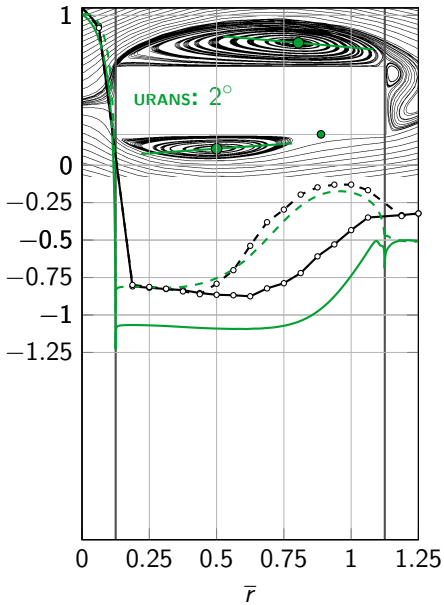
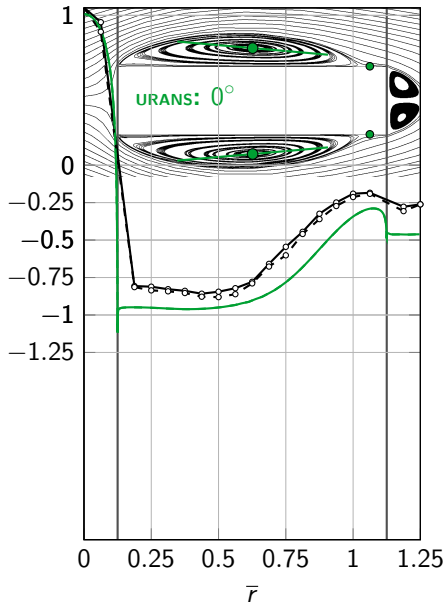
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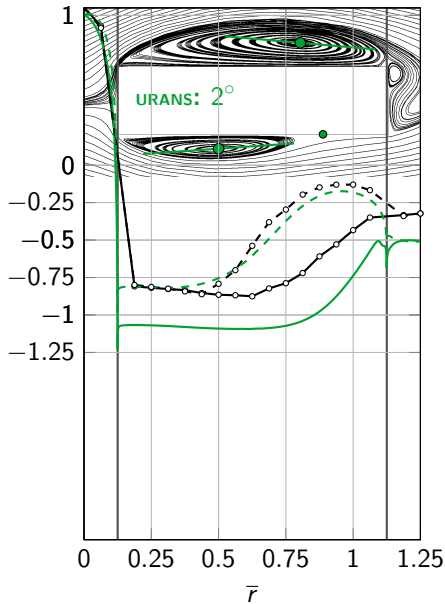
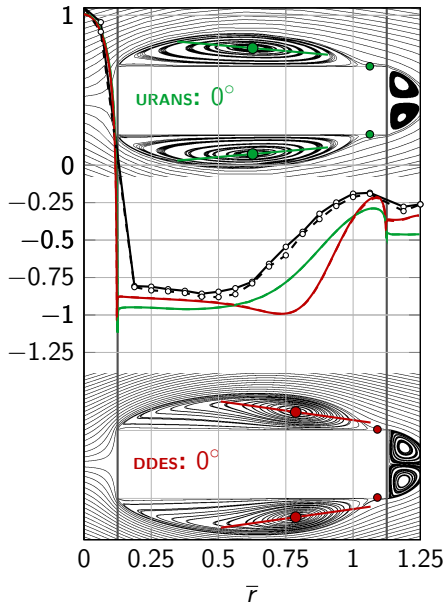
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# Results: $\bar{C}_p$

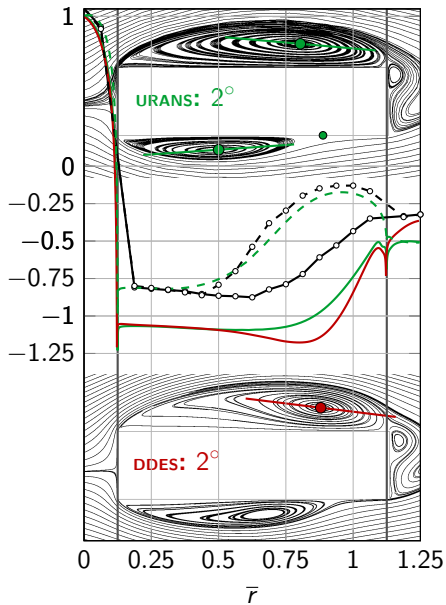
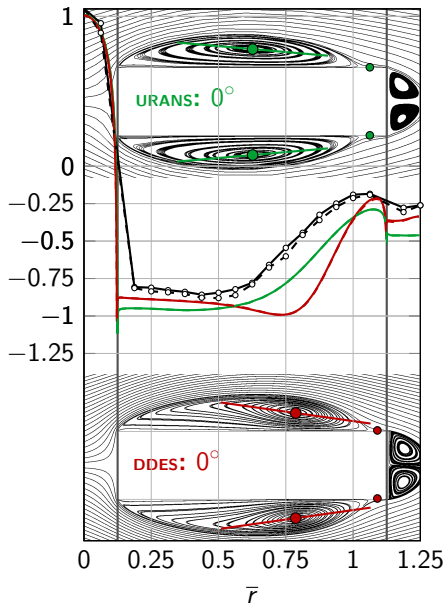




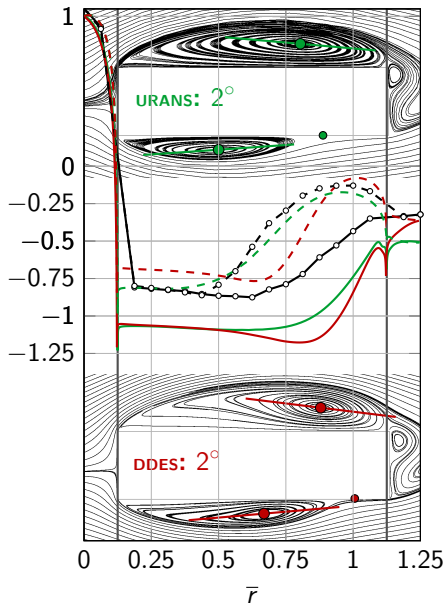
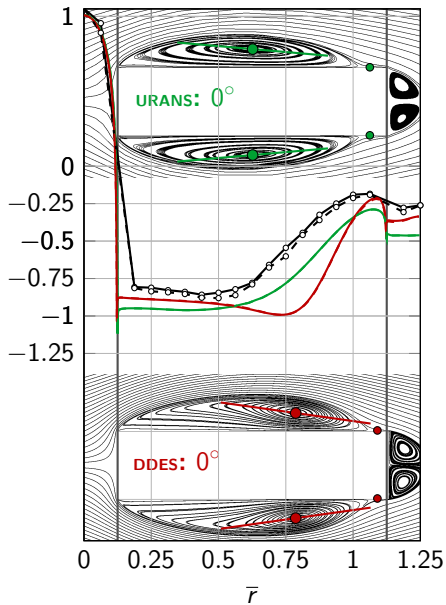
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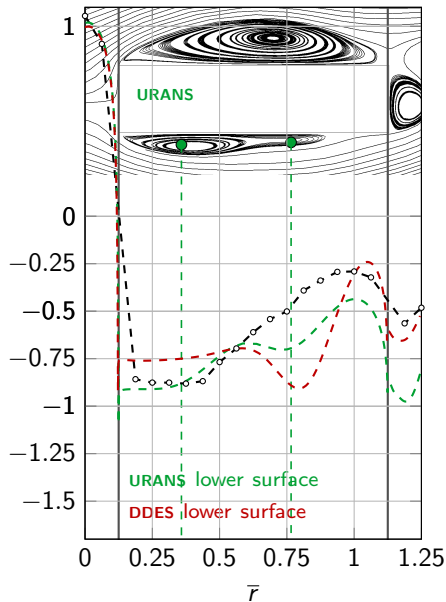
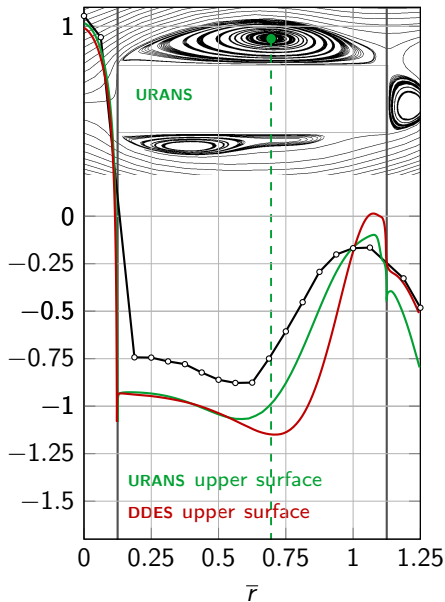
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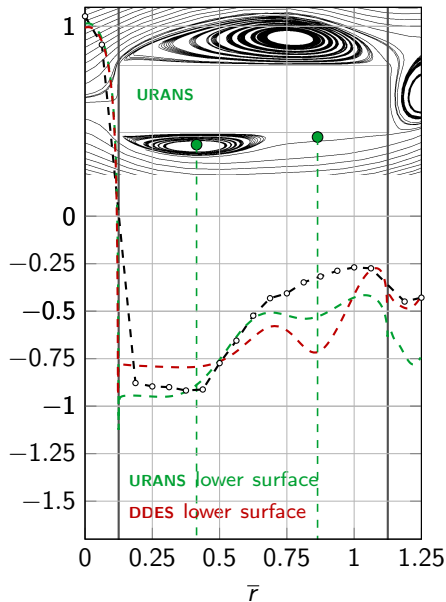
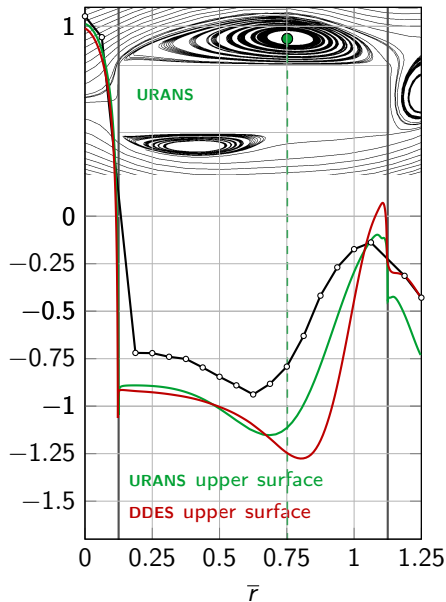
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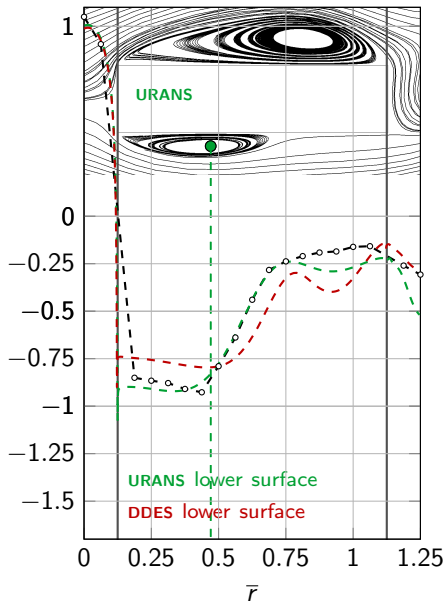
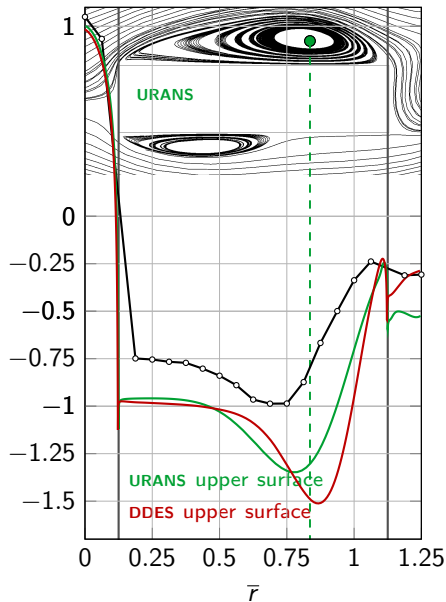
# Results: variation of $\widehat{C}_p$ for $\alpha = 2^\circ$



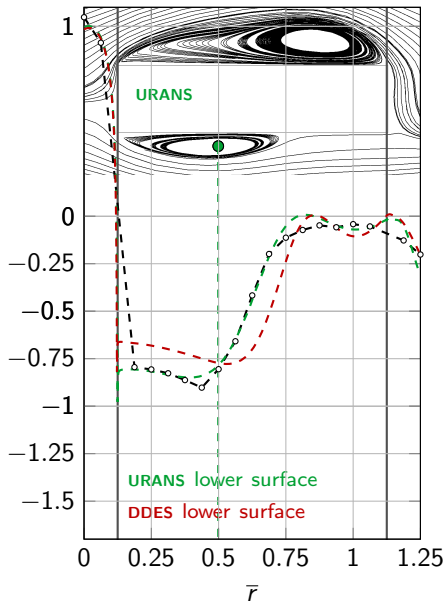
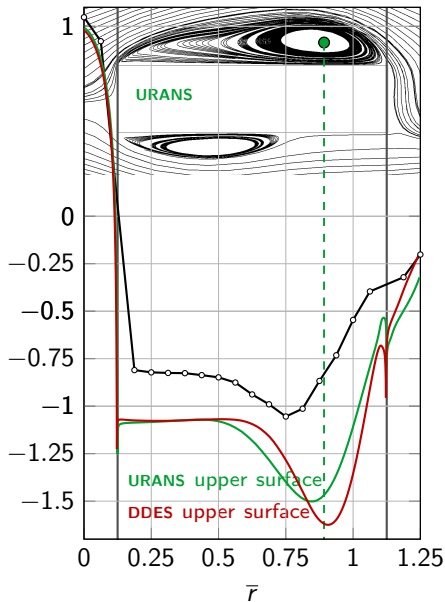
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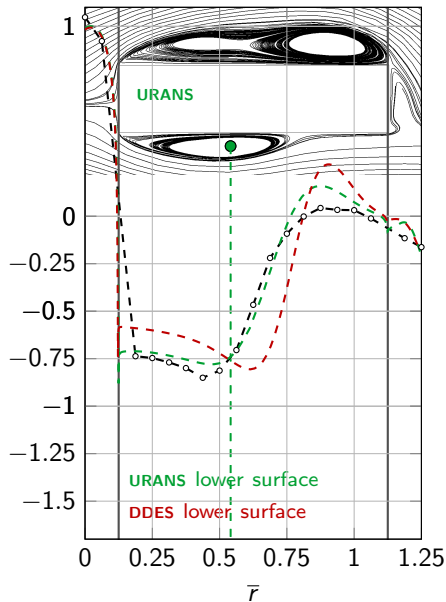
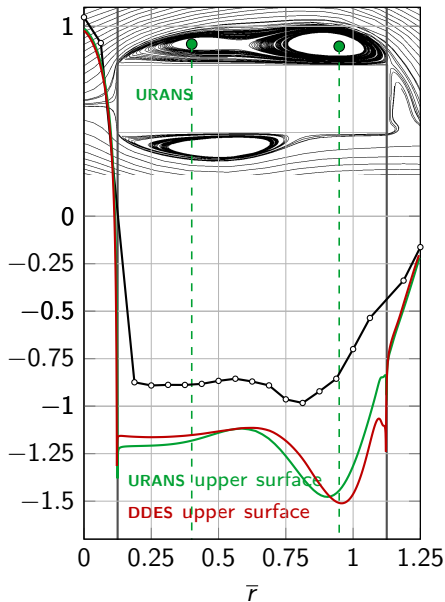
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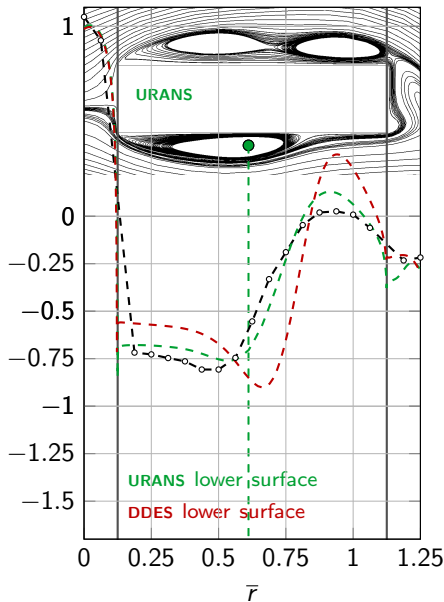
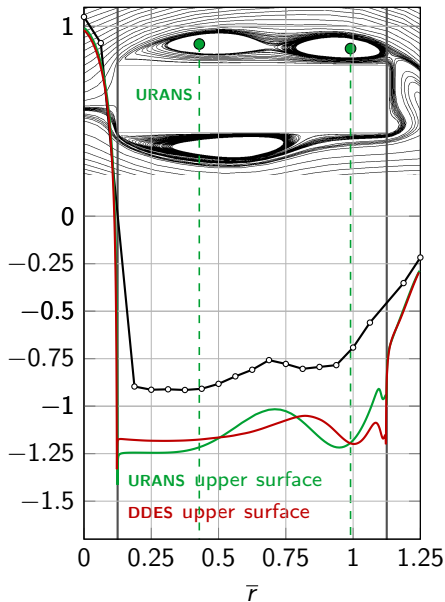


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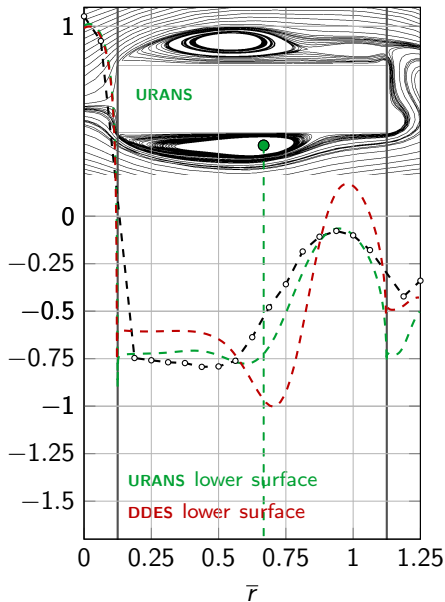
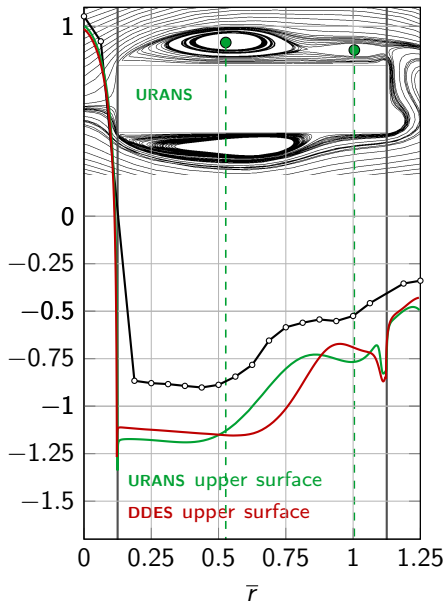




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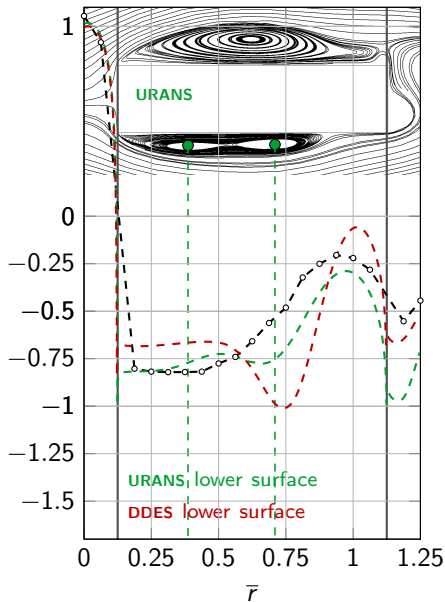
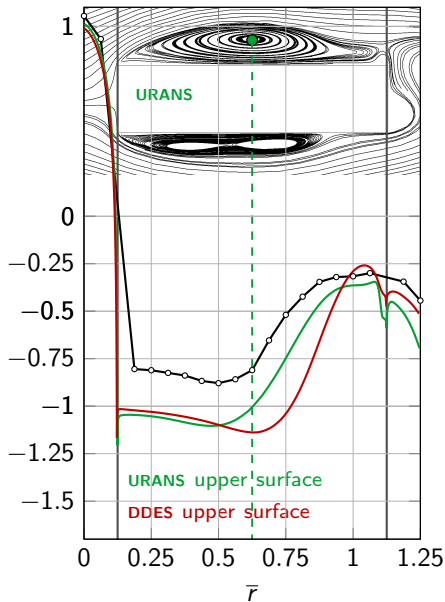


# Results: variation of $\widehat{C}_p$ for $\alpha = 2^\circ$



# Results: variation of $\widehat{C}_p$ for $\alpha = 2^\circ$

$t = 0$



**Conclusion**

# Conclusion

EXP

- $\bar{c}_l, \bar{c}_d, \bar{c}_m$  close to literature
- discrepancies in  $\bar{c}_l$  probably due to Re effects
- flow dynamics extracted using DMD

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EXP

- $\bar{c}_l$ ,  $\bar{c}_d$ ,  $\bar{c}_m$  close to literature
- discrepancies in  $\bar{c}_l$  probably due to Re effects
- flow dynamics extracted using DMD

CFD

- large discrepancies between  $\bar{c}_l^{EXP}$  and  $\bar{c}_l^{CFD}$   
⇒ could be explained by the high sensitivity of the flow  
 $\bar{c}_d$ ,  $\bar{c}_m$  and St are correctly estimated by CFD
- URANS performs better than DDES to capture mean flow and flow dynamics
- only DDES is able to estimate the stall angle

**Thanks for your attention!**

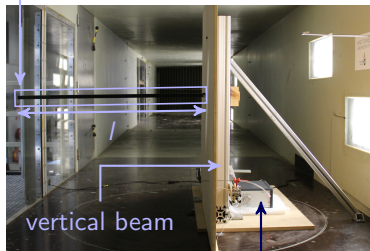
**Additional material**



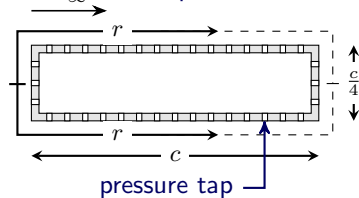
# Methodology

rectangular tube

$$c \times d \times l = 8 \times 2 \times 101 \text{cm}$$



$U_\infty$  pressure sensor



Flow studied through EXP

dynamic pressure measurements  
for different  $Re$  and  $\alpha$

- hollow rectangular tube

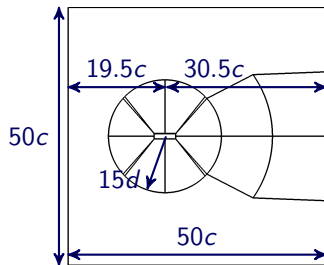
- 36 pressure taps  
(15 along  $c$  and 3 along  $d$ )

- $Re \in [7.8 \times 10^3, 1.9 \times 10^4]$

$\Rightarrow C_p$  for  $\alpha \in [-7^\circ, 8^\circ]$

$\Rightarrow C_l, C_d, C_m$  computed from  $C_p$   
 $St$  through Fourier analysis of  $c_l$

# Methodology



Flow studied through CFD

2D URANS using  $k - \omega$  SST model  
for different  $\alpha$

3D DDES using SA model  
for different  $\alpha$

GRID

- unstructured and structured
- dimensions similar to BARC<sup>d</sup>

URANS

- 75 000 cells
- 1 shedding cycle

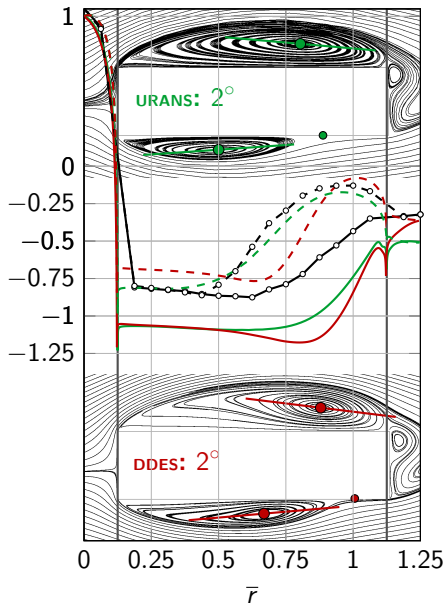
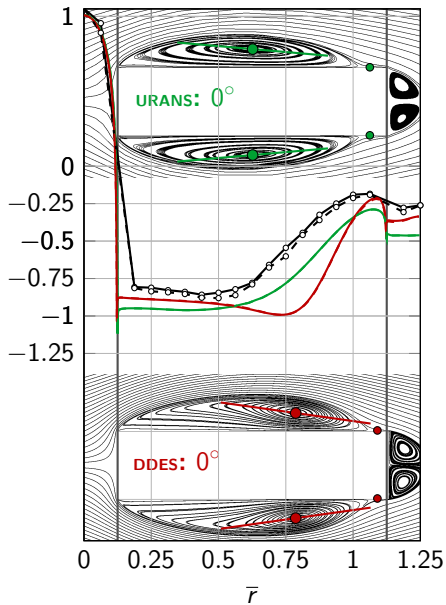
DDES

- along  $z$ :  $1c$  and  $\Delta z = c/64$
- $\Delta_0 = \Delta z$  in focus region<sup>e</sup>  
(extends  $0.5c$  downstream)
- 8 200 000 cells
- 80 shedding cycles

<sup>d</sup>“BARC: An overview after the first four years of activity” by Bruno, Salvetti, and Ricciardelli (2014)

<sup>e</sup>“Young-Person’ s Guide to Detached-Eddy Simulation Grids” by Spalart and Streett (2001)

# Results: $\overline{C}_p$



# Results: $\bar{C}_p$

